



ABSTRACT

The use of open-joint rainscreens, coupled with unconventional wall orientations, can be appealing, but can be a dangerous combination when abating water ingress and compliance with building codes, including combustibility. Balancing the need to keep the building dry, airtight, thermally efficient, and code-compliant can create a cavity wall conundrum. This piece looks at rainscreen design and standards for managing water in the context of the code requiring continuous insulation (ci), air barriers, and water-resistive barriers (WRBs), as well as life safety issues related to combustibility.

Designing exterior walls to be watertight, airtight, thermally efficient, and code-compliant can be quite a balancing act. This is particularly true with modern structures that combine open-joint rainscreens with unconventional wall orientations, such as those that are backward-sloping. In such cases, design teams need to prevent water ingress, but they also must comply with the latest building codes. Staying compliant with recent fire-related aspects of codes, however, can increase potential fire risks.

The American Society of Heating, Refrigerating, and Air-Conditioning Engineers' ASHRAE 90.1 2010 and the 2012 International Energy Conservation Code (IECC), for example, require the use of ci, which in some cases is combustible. The 2012 International Building Code (IBC) requires that buildings in Climate Zones 4 to 7 have a continuous air barrier, which in most cases is also the WRB. All air and water barriers (AWBs), as well as some ci, are combustible, and therefore part of the compliance path (IBC 2012 and later) for National Fire Protection Association (NFPA) 285, *Standard Fire Test Method for Evaluation of Fire Propagation Characteristics of Exterior Non-Loadbearing Wall Assemblies Containing Combustible Components*.

In other words, today's design teams are supposed to be designing building envelopes that are watertight, airtight, thermally efficient, and NFPA 285-compliant. Solving this cavity wall conundrum is possible, but it requires familiarity with competing design challenges and different industry standards and codes. Most cavity wall assemblies have either a metal studs with exterior sheathing or a concrete masonry unit (CMU) backup. All cavity walls share an air space to effectively drain the cavity.

KEEPING THE WATER OUT

According to John Straube, PhD, principal for RDH Building Science Inc., managing water with building enclosures involves the Three Ds: deflection, drainage, and drying. For water to penetrate the surface of a building enclosure, it must first be present on the wall surface. That surface must have an opening through which water can pass, and there must be a force to drive the water inward through the opening.

To quote Dr. Straube, "All leaks occur at holes, but not all holes are leaks." Open-joint rainscreen systems offer an increasingly popular means to achieve the Three Ds.

While the term "rainscreen" is becoming something of a generic phrase, it is important to know there are two main types of rainscreen systems: pressure-equalized (Figure 2), and drained and back-ventilated (DBV) (Figure 3). Both types must control the forces that will carry rain to the inside of the structure, including gravity, surface tension, capillary action, kinetic energy, and pressure differences. The majority of open-joint rainscreens being employed in today's buildings are DBV.

Pressure-equalized

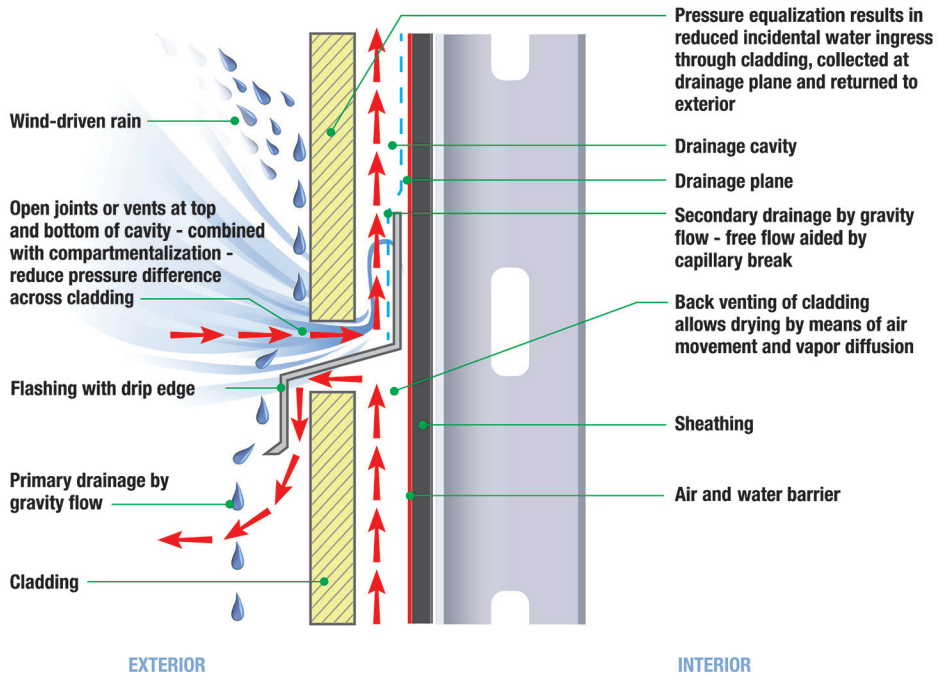


Figure 2 – Pressure-equalized rainscreen systems.

- Open joinery to air, but not water
- Drainable compartmentalization, limiting water pressure disequilibrium
- Complex design, which allows static and dynamic pressure equalization
- Minimizes or eliminates leakage through joints
- Developed in Canada

Behind open-joint rainscreens, AWBs provide the last line of defense against water ingress. There are a number of industry standards to help designers evaluate the water holdout capabilities of an AWB, but not all AWB manufacturers test all their products to each standard. AWB standards include:

- International Code Council Evaluation Service (ICC-ES) Acceptance Criteria (AC) 38, *Acceptance Criteria for Water-resistive Barriers (Sheet Membranes)*, which includes:
 - American Association of Textile Chemists and Colorists (AATCC) 127, *Water Resistance: Hydrostatic Pressure Test*
 - ASTM D779, *Standard Test Method for Determining the Water Vapor Resistance of Sheet Materials in Contact with Liquid Water by the Dry Indicator Method*
 - ICC-ES AC 212, *Acceptance Criteria for Water-resistive Coatings Used as Water-resistive Barriers on Exterior Sheathing*

An additional ASTM standard to evaluate the durability of fluid-applied air barriers (ASTM WK41724, *Standard Practice for Assessing the Durability of Fluid-applied Air and Water-resistive Barriers*) is under development. The task force working on this new standard has been challenged to provide common ground on which the industry can evaluate fluid-applied air barriers, including the water resistance of such barriers.

Once an AWB is installed, there are two other standards building envelope consultants can use to further evaluate the AWB's water resistivity:

- ASTM E331-00 (2016), *Standard Test Method for Water Penetration of Exterior Windows, Skylights, Doors, and Curtain Walls by Uniform Static Air Pressure Difference*
- American Architectural Manufacturers Association (AAMA) 501.2, *Quality Assurance and Diagnostic Water Leakage Field Check of Installed Storefronts, Curtain Walls, and Sloped Glazing Systems*

ASTM E331 is a 15-minute lab test (the field test version is ASTM E1105, *Standard Test Method for Field Determination of Water Penetration of Installed Exterior Windows, Skylights, Doors, and Curtain Walls, by Uniform or Cyclic Static Air Pressure Difference*). The testing consists of using a calibrated spray nozzle that replicates wind-driven rain moving at 3.4L/m²/minute (5 gal/sf/hour), equivalent to 200 mm (8 in.) per hour.

In AAMA 501.2, handheld spray nozzle testing is set at 205 to 240 kPa (30 to 35 psi); there is a distance from the surface of the fenestration of 305 mm (12 in.) for five minutes for each 1.5 m (5 ft.) of joint. This test is best suited for surface-sealed assemblies of nonoperable fenestration.

To evaluate the performance of rainscreens, AAMA has also established AAMA 508, *Voluntary Test Method and Specification for Pressure-equalized Rainscreen Wall Cladding Systems*, and AAMA 509, *Voluntary Test and Classification Method of Drained and Back-ventilated Rainscreen Wall Cladding Systems*.

For these AAMA standards, designers should pay special attention to the amount of water allowed to get into these rainscreen systems while still being considered “passing.” Under AAMA 508, if the area of the water mist or droplets is greater than five percent of the AWB surface, it is considered a failing system. Under AAMA 509, water is expected to reach the WRB, so the pass/fail measure is whether the system is capable of venting and drying over time. Again, the AWB is the last line of defense for water getting into the building. As such, this system needs to be a robust, fully adhered, and properly designed, detailed, and constructed system.

Designers should also consider the cladding attachment system and its location relative to the ci, as this influences the choice and thickness of the AWB. When the cladding attachment system is outboard of the ci, the fasteners that hold the cladding support brackets will penetrate the ci and the AWB without compressing the AWB. In such cases, an AWB that is an adhesive-backed sheet membrane offers a robust solution, as the adhesive clings to the fastener shank, helping seal the penetration.

If the cladding support system is fastened directly through the AWB and then into the exterior sheathing before going into the structural support, either an adhesive-backed sheet membrane or a full-bodied, fluid-applied material performs well.

MAKING IT AIRTIGHT

Air barriers have been part of the National Building Code of Canada (NBC) since 1985. In the United States, air barriers were first adopted in the State of Massachusetts Building Code in 2000. For many other states, air barriers began to gain recognition with designers when the code of record became the 2012 IBC, which requires a continuous air barrier inclusive of the roof. Considerations for evaluating and specifying air barrier systems include vapor permeance and airtightness.

VAPOR PERMEANCE

Proper vapor permeance is determined by several parameters, including climate zone, interior relative humidity (RH), and the mechanical system (and whether it is designed to provide a positive or negative pressure).

If you find yourself still scratching your head, you can always perform a hygrothermal analysis using WUFI software or other similar programs. Analysis with WUFI can provide a calculation of the transient hygrothermal behavior of multi-layer building components exposed to a local natural climate condition.

Determining the proper vapor permeance can be a bit of a conundrum, and ASTM does not simplify matters. For example, ASTM E96, *Standard Test Methods for Water Vapor Transmission of Materials*, has multiple test procedure options. The two test procedures primarily used in our industry are Procedure A – Desiccant Method, and Procedure B – Water Method. Essentially, both procedures use the same test apparatus, temperature, and RH, but Procedure A utilizes a cup with a desiccant in it and is weighed once equilibrium is reached (water vapor entering the cup). Conversely, Procedure B utilizes a cup with water in it, and once equilibrium is reached (water vapor leaving the cup), the remaining water is weighed. The two procedures can yield significantly different results.

The International Code Council (ICC) recognizes Procedure A. When the Air Barrier Association of America (ABAA) evaluates air barriers, they perform and publish the results for both Procedure A and Procedure B. There is an ASTM specification guide under development (WK51917, *Specifying Water Vapor Transmission Properties of Water-Resistive Barriers and Air Barriers*). This group contends that given the position in the wall assembly (beneath the clad-

ding, protected from direct sun and wind-driven rain), the AWB is exposed to environmental conditions similar to the exterior environment, and unless the project is in the arid desert, Procedure B is more relevant.

AIRTIGHTNESS

There are a few different ways to evaluate an air barrier, and these are also the same compliance paths in IBC and IECC. To be compliant with both codes, an air barrier needs to pass one of the following evaluation methods, listed in order of magnitude.

Material Testing

ASTM E2178, *Standard Test Method for Air Permeance of Building Materials*, is a pass/fail test at the threshold of $0.02 \text{ L}/(\text{s m}^2) @ 75 \text{ Pa}$ ($0.004 \text{ cfm}/\text{sf} @ 0.3 \text{ in. w.c.}$). This test is based on the air permeance of 13-mm ($\frac{1}{2}$ -in.) gypsum. While it is fairly easy for materials to pass, as with all tests, it is important that the air barrier manufacturer has the evaluation performed by an accredited third-party testing facility.

Assembly Testing

ASTM E2357, *Standard Test Method for Determining Air Leakage of Air Barrier Assemblies*, is more rigorous than ASTM E2178, as it evaluates an entire assembly rather than just the AWB material. Since it is performed in a lab, manufacturers can use fastener cap washers, tapes, and sealants not typically employed in the field to pass the test. This is a pass/fail test in which an opaque wall is evaluated against one with a mock window buck, penetrations, and an outlet. The air barrier system is also terminated at what would be the foundation and the roof.

Drained and Back-ventilated

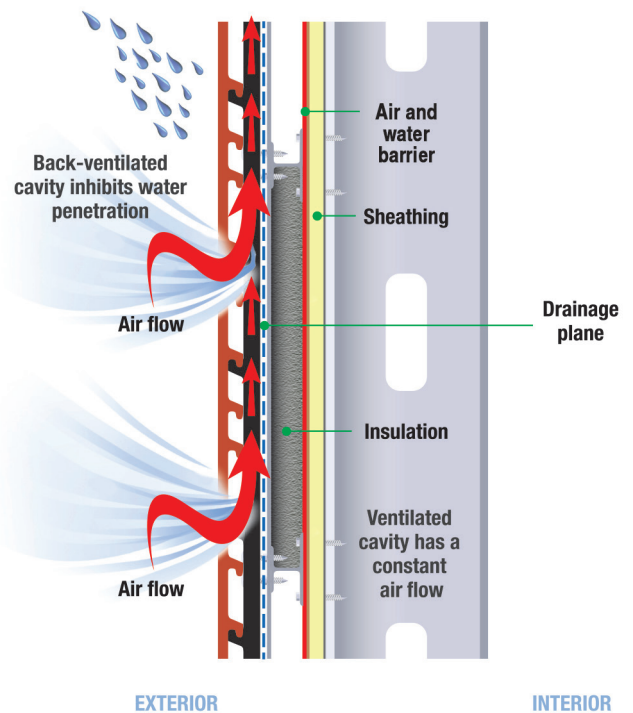


Figure 3 – Similarities and differences between pressure-equalized and drained and back-ventilated rainscreen systems.

- Open joinery; cladding is allowed to leak
- Drains most of the water at outer cladding
- Relies on cavity ventilation to drain and dry residual water
- 25-mm (1-in.) gap for brick cladding; 13-mm ($\frac{1}{2}$ -in.) minimum gap for other claddings
- Requires robust, continuous, properly flashed air and water barrier
- Not pressure equalized
- Developed in Europe

The sample walls are put under sustained cyclic and gust loads, replicating worst-case conditions. If the wall with the penetrations leaks more than 10 percent at 75 Pa versus the opaque wall, it fails. When ABAA evaluates air barrier products, part of the assessment includes ASTM E2357. The association uses $0.20 \text{ L}/(\text{s m}^2) @ 75 \text{ Pa}$ ($0.04 \text{ cfm}/\text{sf} @ 1.56 \text{ lb}/\text{sf}$) as its pass criteria.

Whole-building Airtightness

ASTM E779, *Standard Test Method for Determining Air Leakage Rate by Fan Pressurization*, is the gold standard in air barrier performance testing. The U.S. Army Corps of Engineers (USACE), having proven airtight buildings offer profound energy savings, has required ASTM E779 for several years. The standard requires testing the

building @ 75 Pa. However, while a material can leak at 0.02 L/(s m²) @ 75 Pa (0.004 cfm/sf @ 0.3 in. w.c.), an entire building can only leak at 2 L/(s m²) @ 75 Pa (0.4 cfm/sf @ 0.3 in. w.c.). USACE lowers the standard to 1.25 L/(s m²) @ 75 Pa (0.25 cfm/sf @ 0.3 in. w.c.).

This whole-building airtightness standard is showing up in more building codes. Additionally, there is an uptick in passive house designs in commercial buildings. Passive houses take ASTM E779 to a whole new level where the air leakage standard is 0.6 ACH (air changes per hour) @ 50 Pa (0.6 ACH @ 50 Pa = 0.03-0.15 CFM/ft²@75 Pa).

THERMAL RESISTANCE AND CI

Beginning with the 2012 IECC, ci is required in all above-grade walls for all climate zones (Figure 4). ASHRAE 90.1, *Energy Standard for Buildings Except Low-rise Residential Buildings*, defines ci as: “Insulation that is uncompressed and continuous across all structural members without thermal bridges other than fasteners and service openings.”

Stuffing insulation between Z-girts is not consistent with ASHRAE 90.1. If a project uses horizontal girts, they should be shimmed from behind so water is free to run down the AWB and not become trapped.

Although spray polyurethane foam (SPF) and expanded polystyrene (EPS) are used as insulation in cavity wall assemblies, thermoplastic extruded polystyrene (XPS) is a much more prevalent ci. XPS is a thermoplastic rigid foam insulation board. As a combustible thermoplastic polymer, XPS generally melts and drips prior to ignition when exposed to a fire source.

Due to its fundamental combustion properties, XPS is not used behind combustible claddings in cavity wall systems that must pass NFPA 285 for resistance to fire propagation. In such situations, mineral wool or fire-enhanced polyisocyanurate (polyiso) must be used instead. For noncombustible-cladded NFPA 285 assemblies, XPS is a realistic option, as the masonry or other noncombustible cladding provides adequate fire protection.

XPS also has the highest resistance to water absorption of any type of foam plastic insulation, allowing it to maintain its R-value in wet cavity wall locations. According to the Extruded Polystyrene Foam Association (XPSA), the aged R-value of XPS at 50 mm (2 in.) is R-5.0 per inch @ 24°C (75°F).

Since polyiso is a thermoset plastic, it is less susceptible to burning than XPS, but will char and smolder when exposed to fire. This behavior enables certain types of polyiso, with additives in the foam, to be used behind combustible claddings and

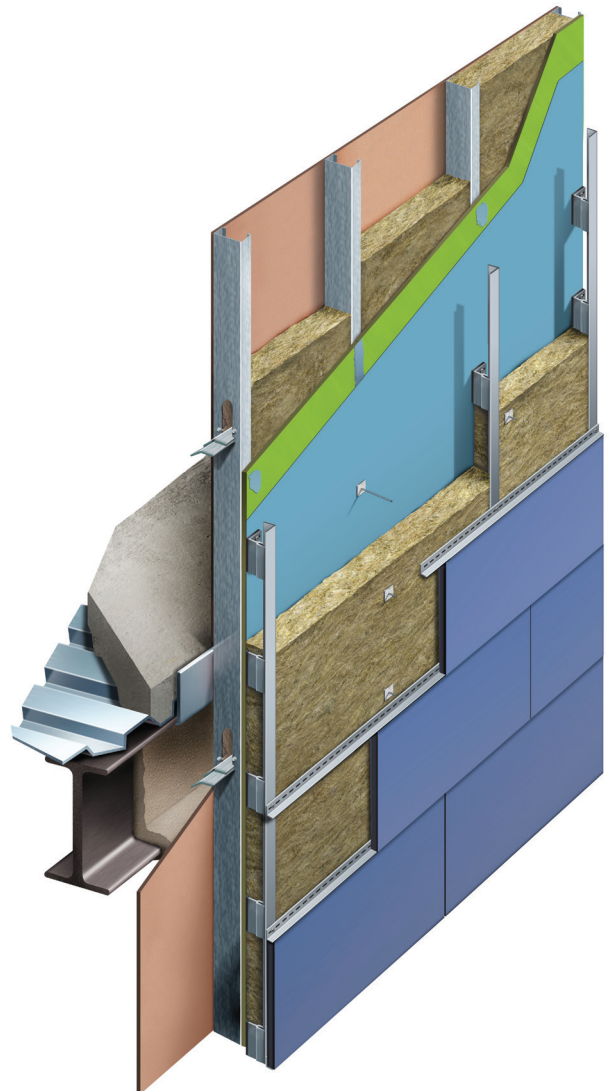


Figure 4 – Mineral wool continuous insulation. Image courtesy Owens Corning.

pass NFPA 285. Designers should check with the manufacturer to verify the polyiso under consideration is suitable for such

RCI Interface Seeks Project Profiles

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RCI Interface is particularly interested in submission of project profile articles concerning unique building envelope projects. Profiles should be 1500 to 2500 words with five to 15 high-quality photos and should describe a building issue that is diagnosed or solved or an unusual building or condition worked on in the course of a building envelope consultant's work. Submit articles to Executive Editor Kristen Ammerman, kammerman@rci-online.org.

applications. According to the Polyisocyanurate Insulation Manufacturers Association (PIMA):

Among all foam plastics, polyiso possesses the highest level of inherent fire resistance due to its unique structure of strong isocyanurate chemical bonds. These bonds result in improved high-temperature resistance (up to 390°F [200°C], more than twice the temperature resistance of other building insulation foams), which in turn leads to enhanced fire resistance.

It is uncommon to see more than a 76-mm (3-in.) layer of polyiso pass an NFPA 285 test with a combustible cladding. The aged R-value of foil-faced polyiso, per ASTM C518, *Standard Test Method for Steady-State Thermal Transmission Properties by Means of the Heat Flow Meter Apparatus*, at 50 mm (2 in.) is 6.25 to 6.5 per inch.

For NFPA 285 compliance, mineral wool offers designers a get-out-of-jail-free card. Offering a heat resistance of 850°C (1562°F) and a melting point of 1177°C (2150°F), mineral wool essentially will not burn. Mineral wool is not limited by thickness, so any thickness of insulation can be installed and maintain compliance. Mineral wool has a flame spread and smoke developed rate of zero per ASTM E84, *Standard Test Method for Surface Burning Characteristics of Building Materials*. The R-value of one manufacturer's exterior wall product ranges from R-4.0 to R-4.3 per inch.

NFPA 285 COMPLIANCE

Perhaps the most vexing element of cavity wall design is compliance with NFPA 285. As defined by the NFPA, the standard is a *Standard Fire Test Method for Evaluation of Fire Propagation Characteristics of Exterior Non-loadbearing Wall Assemblies Containing Combustible Components Using the Intermediate-Scale, Multi-story Apparatus*. (Prior to its IBC adoption in 2000, a similar, larger-scale test appeared in the 1988 Uniform Building Code [UBC].) The code applies to Type I through Type IV construction on multistory projects, or single-story walls in excess of 12 m (40 ft.).

The defining characteristic of NFPA 285 is that it is an assembly test (Figure 5), just like a UL or Factory Mutual (FM) roof assembly test. A manufacturer may market an air barrier as "fire resistant" or "fire rated,"

but such designations have no bearing on compliance with NFPA 285. Complicating matters, there is no single clearing house to provide designers with tested and passed assemblies.

In the late 1980s, NFPA required exterior insulation and finish system (EIFS) manufacturers to test their systems. Other foam plastic insulation manufacturers (e.g., those involved with XPS) have been vigilant with their testing for years, and have very thorough reports of assemblies with which their

products comply. In the 2012 IBC, AWBs had to comply with Section 1403.5, as all AWBs are combustible. However, when some states and the District of Columbia adopted the 2012 IBC, they excluded 1403.5.

According to the 2015 IBC, 1403.5 can be excluded if the AWB is the only combustible component in the assembly. The 2015 IBC also specifies if the AWB falls below a certain level of fuel contribution (based on ASTM E84 Class A and ASTM E1354, *Standard Test Method for Heat and*

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Visible Smoke Release Rates for Materials and Products Using an Oxygen Consumption Calorimeter), and it is the only combustible component in the assembly, it will not require NFPA 285 compliance. Further, rough opening flashings associated with the AWB system are also excluded from NFPA 285 compliance requirements.

Ultimately, NFPA 285 compliance is all about preventing loss of life. Recall the case of the 72 people who perished in the Grenfell Tower in London on June 14, 2017. The cladding on this building was aluminum with polyethylene foam insulation core. Inside of the cladding was a 50-mm ventilation space. Secured to the existing cladding was 150-mm polyisocyanurate insulation. The cavity wall assembly

in the Grenfell Tower would not comply with NFPA 285. Accordingly, the United Kingdom Parliament has committed £400M (about \$536M) to remove all “Grenfell-style” cladding from high rises in the United Kingdom.

THE CAVITY WALL BALANCING ACT

While each of the preceding topics could be expanded into an article of its own, they are highlighted here to help make building designers aware of the competing requirements and standards involved in modern cavity wall design. Designers should know that continuous air barriers and continuous insulation, along with NFPA 285, are code-compliance issues that must be balanced with the goal of keeping water out of the building. Achieving this balance will

help designers go a long way toward designing the safest, most energy-efficient building envelopes possible. 



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Swiss University Fabricates World's First Full-Scale 3-D Sand Printing Architectural Project

Researchers at ETH Zurich University in Switzerland have developed an innovative 3-D sand printing technique with which they have fabricated their first full-scale concrete slab. The 80-square-meter (861-sq.-ft.) slab at the DFAB House, dubbed the “Smart Slab,” carries a two-story timber unit above it.

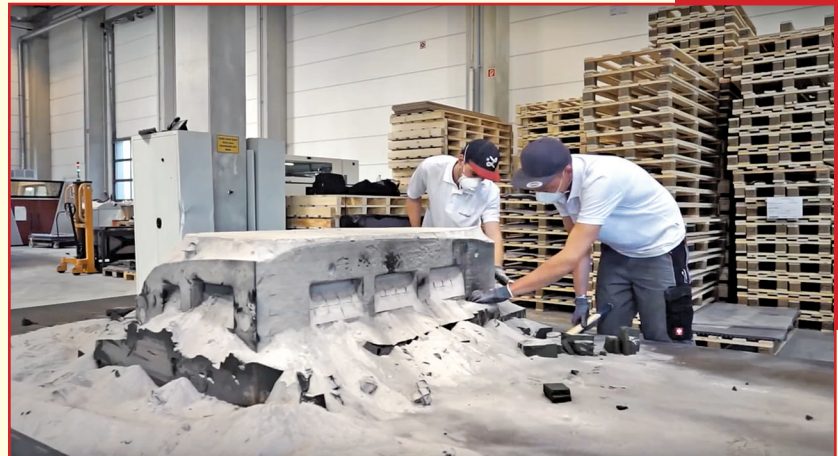
The intricately designed ceiling maintains load-bearing characteristics with precision narrowed down to millimeters. The software coordinated and recorded all the parameters of the room. After the forms were created, the sand mold was sprayed with fiber-reinforced concrete, creating an organic, ribbed surface. The team then cast the remaining concrete into the timber form-work, creating the final form. Following completion, the mold can be dismantled and reused for other projects.

Eleven segments were allowed to harden for two weeks, and then they were transported to the designated site and installed using a crane and steel cables to pre-stress the concrete mold into the structure.

To view a video of the process, visit: https://www.youtube.com/watch?time_continue=17&v=FUw3MWhD9dY.

— Archdaily.com

Installation of Smart Slab on DFAB House in Zurich, Switzerland.



Researchers make 3-D-printed sand mold at ETH Zurich.

